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OUR COVER

An engineer is shown testing a versatile two-channel tape recorder exhibited at the recent International Audio Festival and Fair in London. This new professional transportable recorder is equally suitable for recording chamber music as the roaring blast of a jet aero engine. (Photo by courtesy of the United Kingdom Information Service in Australia.)

FEDERAL COMMENT

★

I.T.U. PLANNING

As another year draws towards its close, we come nearer to the next I.T.U. Conference. Although a definite date has not yet been set for its time or venue, present indications are that it will probably be held some time in 1965. Irrespective of when it would commence, some discussion took place at the recent Federal Convention in Perth as to the Institute's preparedness for this event and what Federal Council action was to be taken.

It is obvious to every Amateur who stops to think about it that Amateur frequencies will again be under fire from other Services and will probably be harder pressed than in 1959. We came out of the last battle reasonably well when everything is considered, but we can ill afford to be complacent about our status in Australia or the support of our American contemporaries. We must be prepared to fight our own battles. We can only do this effectively if we again send a representative to Geneva or wherever the Conference is to be held.

No one will deny that we may have fared a lot worse if the late John Moyle had not been present in Geneva to represent the Institute and carry our battle into the front line. His personal diplomacy, discussions behind the scenes with other representatives, lobbying where necessary and particular knowledge of all the problems involved were contributing factors in the Australian Amateur's rise in status with the authorities and the at least partially successful prosecution of our aims.

It is therefore equally true that we must be represented once more, and to this end, planning is already in hand to determine the best and most effective way of again raising sufficient funds to send another representative. Who this representative may be is a matter for the future but you may rest assured that we will again have the best man that is available at the time. This is, however, not our main concern at this juncture—we must first raise sufficient funds to enable us to send one.

Premature action in any fund-raising scheme of this nature can easily kill it if it is not properly organised, although donations at any time for this purpose would always be welcomed. But until this has been fully discussed by Federal Council and a policy determined, individual organising attempts may be largely wasted. We know from past experience that when the case is put fairly and squarely before the average member and non-member, he will rise to the occasion as he did before, and give his wholehearted support to the financing of the representative to protect his interests and hobby. At the appropriate time, the "green light" will mark the opening of a nation-wide appeal.

—FEDERAL EXECUTIVE, W.I.A.

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MATTERS—MOBILE

PART TWO

K. WOODWARD,* VK2ZAU

MOBILE AERIALS

V.H.F. AERIALS

If the previous sections have not caused fires of wrath to descend upon the author's head, this should finish the job. Firstly, we will tackle the problem of v.h.f. aerials. The simplest mobile aerial is a quarter wave whip (not on 7 Mc. please) and a short discussion on achieving the best results from these will not be out of place.

The impedance of a ground-plane aerial will give good matching when fed with 39 ohm coaxial cable. This cable is commercially available, but should your Scots blood prevail, use two lengths of 72 ohm coax. In parallel, the approximate lengths for quarter wave whip on 50 and 14 Mc. are 55 and 19 inches respectively.



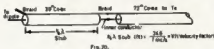
Now should you wish to use 52 or 72 ohm coax. to feed your whip, you can do so and achieve very close matching with the following method. As illustrated in Fig. 18 a variable capacitor is placed in series with the inner conductor feed to the whip, but the length of the whip must be altered. The approximate lengths will be—50 Mc.: 52 ohm coax., 56½"; 72 ohm coax., 73½". 14 Mc.: 52 ohm coax., 23½"; 72 ohm coax., 25½". The whip should be adjustable in length and varied as well as the variable capacitor to give maximum radiated field strength. This is, of course, where your field strength meter will be invaluable.

When testing a ground plane aerial use a vertical whip on the field strength meter, and when testing beams (horizontal) use a horizontal dipole. When you make an adjustment to your aerial do not forget to re-peak your transmitter output, watching the field strength meter for maximum output.

For field days you will want to make provision for v.h.f. beams and Fig. 19 illustrates the one used by the author with considerable success. This beam converts from 2 metres to 6 metres for stationary operation, but the 2 metre

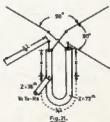
section has travelled at 50 m.p.h. on country roads. The original beam has snap-in type elements, but there is no reason why extension pieces could not be engineered for the radiator and D2 of the 2 metre beam.

A folded dipole as the radiator would give a good match to 72 ohm coax. feeder, but the author prefers the original method of matching with a quarter wave stub. This stub, illustrated in Fig. 20, is made of 39 ohm coax., the lengths being—50 Mc., approx. 39"; and 144 Mc., approx. 13½". In practice, except for the most stringent conditions, the 50 Mc. stub is left on permanently as it does give a fair match on 144 Mc.



The velocity factor for coaxial cable can be taken as 0.66 when calculating the quarter wave stub. The four element beam on two metres will give an approximate power gain of eight times, and if designed for 50 (with the 0.2 wavelength spacing) would make an excellent home station beam. The two element beam on 50 Mc. gives an approximate power gain of three times.

In v.h.f. mobile aerials, one which has no gain but permits fairly circular horizontal coverage is the turnstile. This aerial illustrated in Fig. 21 is simple to make and to match, and will give better results than a quarter wave whip when working horizontally polarised home stations. Incidentally, at least one Sydney home station has been using a similar aerial on 2 metres with very good results. The two distances X are not important as long as they are of equal length. The correct phasing being achieved by the extra quarter wavelength on one set of dipoles. This quarter wavelength should be calculated as for a quarter wave stub and would be approximately 13½" at 144.5 Mc. The feeder cable could be two parallel lengths of 72 coaxial cable.



To finish the discussion of v.h.f. aerials, it must be pointed out that the most efficient position for a whip is in the middle of the roof. If you do not wish to cut a hole in your roof, it may be possible to fix a metallic base plate to your whip and fasten it to the roof with rubber suckers. Remember that

if you mount the whip on your mudguards endeavour, wherever possible, not to get your car body between the whip and the station being worked.

First choice is the roof, second choice can often be the centre of the boot lid, third choice is the mudguards. If you have an external metallic sunvisor these often make a good mounting place for a v.h.f. whip. When sitting your whip other than on the roof, try for a removable ornament or drill your holes so they can be used for a normal car aerial or side-vision mirror, etc., when the car is to be sold.

7 Mc. AERIALS

A book could be written on this topic alone as there are so many approaches to the manufacture of an efficient 7 Mc. mobile aerial. Firstly, the spiral whip, secondly the base-loaded whip, and thirdly the centre-loaded whip. We will deal only with the centre-loaded whip. The most important factor in this aerial is the loading coil. It should have the highest possible Q with smallest dimensions, thus reducing to a minimum air-resistance.

We will assume a whip of 8 feet, 3 feet at the base and 5 feet above the loading coil. The loading coil suggested for 40 metres is approximately 32 microhenries, wound as follows: 30 turns of 14 gauge enamelled wire, 24" diameter, approximately 5" long. This coil should ideally be air-wound, rib supported. However, should this be impossible, the best insulator possible should be used, polystyrene, etc., remembering any loss in this coil makes a very big loss in radiation efficiency.

With the aerial installed and the transmitter operating, the top section of the whip should be adjusted to give maximum radiated signal. If the coil has been wound correctly, this need not be touched, however in no circumstances whatever leave a shorted turn on the coil or introduce any unnecessary metallic objects. Remember after each adjustment to the whip, to re-peak your transmitter before noting the exact radiated field strength.

The approximate radiation resistance of this whip, depending on installation, will be 10 ohms, so you will readily appreciate that there will be a mismatch with any coaxial feeder used. This can be overcome by placing a capacitor from the base of the whip to ground. It may be necessary to add a turn or two to the centre loading coil, but the necessary adjustment can usually be made by the top section of the whip.

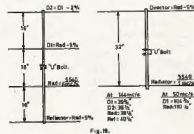
The size of the condenser depends on the impedance of the coaxial cable and the impedance of the aerial, the formula for determining this being as follows:—

$$C = \frac{2 \times \pi \times f \times R_a \times R_s}{10^9}$$

where R_a = impedance of aerial.

R_s = impedance of feeder.

Assuming an aerial impedance of 10 ohms and a feeder of 50 ohms at 7 Mc., the condenser value would be 1,099 pF.



* Flat 28, Block 3, Curtis Place Flats, Moorehead Street, Redfern, N.S.W.

Having spent the time to make up this aerial and tune it correctly, should reward you with many pleasant QSOs. Remember that this aerial has a high Q and should be resonated on your favourite operating frequency. If your transmitter is v.f.o. controlled, you can check the exact resonance point of your aerial and operate within ± 30 Kc. of this point for best results.

This is the last of this series of mobile equipment and we will discuss briefly the fundamental basis of all mobile operation, the power supply.

TRANSISTOR P.S.

I do not intend to give a circuit for a transistor power supply as an excellent one has been featured by Mullard and details, if not at hand, can be obtained from that company at no obligation. Moreover, the transformer for this power supply, the thing which most people like myself are too lazy to manufacture, may be purchased from a local transformer manufacturer (an advertiser in "A.R.") for a reasonable sum. Also you may purchase a complete power supply from two or three sources which give satisfactory results. Whatever your approach, it is handy if possible to obtain a tapped power supply of at least one high and one medium output voltage. It is possible to run your power supply at a lower output voltage with much lower primary current drain than when transmitting at high h.t. voltage.

Never abuse your transistor power supply. Mount it so that it receives, if possible, a good flow of air current, not possible at least make sure it is not subjected to a great deal of heat from external sources. Make sure that you connect the correct polarity to the supply and if purchasing same ask for the facility, and the instructions how to, of changing the polarity input—remember you may sell your car some day.

If the power supply is not fused make sure you insert the correct size fuse in the 14. lead. Normally a transistor power supply fails safe if incorrectly treated, but do not rely on this feature; you may be unlucky and power transistors are not cheap. Although not so critical as vibrators to car voltage, take care that your regulator system is working correctly and the charging voltage is not exceeding approximately 14 volts.

In manufacturing any type of power supply I do recommend the use of silicon rectifiers, OA210s, etc. Most power supplies these days use voltage doubler circuits, thus saving a little

space and weight as far as the transformer is concerned, especially if you are hand-winding same! Illustrated in Fig. 22 is the output filtering and voltage doubling circuit as used in a commercial power supply. The electrolytic condensers are dual types. The reason for the simple filtering is, of course, that the supply is working at audio frequencies, not 50 cps. Should the wave voltage doubling circuit be used with a vibrator supply, it may be necessary to replace the first 27 ohm resistor with a choke to obtain efficient filtering.



The big advantage of the transistor power supply over than conversion efficiency is the absence of radio noise at short wave frequencies as compared with the genemotor and vibrator power supplies. However, do not be surprised if you try to listen to your portable wireless in the car if you get several birdies on the broadcast band from the transistor power supply.

The following adaption for a genemotor supply was extracted from VK-2ZVL by gentle persuasion to horrible record in this magazine. VK2ZVL has been using this idea for some years very successfully on the v.h.f. frequencies. Nearly everyone is familiar with the I.F.F. style genemotor designed for operation of 18 volts but which functions quite well on 12 volts. However, the output voltage of 250 or less, depending on the design, does not seem to be desired. Fortunately this can now be remedied with a little work on the input side of the genemotor.

As can be seen in Fig. 23 a third brush holder (insulated) has been fitted to the l.t. input of the genemotor. No wiring changes are to be made. It is simply necessary to ground the original terminal for reception and change this ground over to the new brush holder terminal during transmission periods. The third brush position should be adjusted for best output voltage before fastening securely to the genemotor frame.

I stress that the third brush be used for intermittent transmitter use only, as



depending on the position of the third brush the generator could be run to destruction in approximately one hour continuous running on the third brush due to overheating. This method, however, is OK for normal mobile transmission periods excluding the fox on fox hunts.

Having mentioned the subject of fox hunts, brings us to the first topic in the miscellaneous items, the fox-hunting aerial for 2 metres.

Fox-hunting beams are constructed for maximum back-to-front ratio and whilst most beams used seem to consist of three elements with 0.1 director spacing and 0.15 reflector spacing, the author is not fully in agreement with this system. I prefer a three element beam with 0.1 director spacing and 0.25 reflector spacing, however the element lengths are not cut to standard length as for maximum gain.

The director should be approximately 10% shorter than the radiator and the reflector approximately 7½% greater than the radiator. A sample beam cut for 144.5 Mc. would then be as follows: Director 34½", radiator 36½", reflector 41½"; director spacing 8" and reflector spacing 20". The result looks horribly unbalanced but performs well. A very rough match can be made to coaxial cable with a folded dipole radiator and seems good enough for the purpose of fox-hunting.

In chasing hidden transmitters you must be able to turn your receiver gain right down, preferably at the front-end otherwise when you get very close to the fox you will not be able to get a reasonably true bearing. Of course a good S meter or magic eye is virtually a must. Maybe someone with a good deal of experience in this field will contribute an article on how to beat the experts.

I understand an excellent article on mobile switching, road safety, aerial efficiency, and layout of mobiles is shortly forthcoming, so we will leave these subjects to our fellow author. ●

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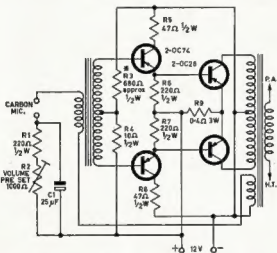
MODIFICATIONS TO MODULATOR DESIGN WITH OC26 TRANSISTORS*

It has been found that under unfavourable circumstances—particularly under sustained drive—the previously described ("Mullard Outlook", Australian Edition, Vol. 3, No. 3, pages 28, 29 [also "A.R." May '61—Editor "A.R."]) "Modulator Design with OC26 Transistors" may be thermally unstable. Leakage currents in the OC74 driver transistors and in the OC26 output transistors may be equally responsible. To guarantee thermal stability under sustained-drive conditions at ambient temperatures of up to 48°C, it is recommended that the following modifications be made:—

Revised Performance Figures

Maximum output power, 1,000 c/s. (10% total harmonic distortion)	14.5 W.
Voltage across input terminals for maximum output power	920 mV.
Input impedance (approx.)	50 ohms
Negative feedback	9 db.

The above concludes the extract from "Mullard Outlook", Australian Edition. Below is an extract from "Info." (VK5 Division Bulletin).



- (a) A resistor of 0.4 ohms (R9 in the accompanying circuit diagram) should be included in the common emitter return of the output transistors.
- (b) To minimise heating of the driver transistors under drive, 47 ohm collector load resistors (R5, R8) should be used.
- (c) The return resistors for OC74-emitter-OC26-base (R6 and R7) should be decreased from 1.2K ohms to 220 ohms.

It should, in addition, be ensured that the 2-OC74 as well as the 2-OC26 have adequate heat sinks—the cooling fins being screwed on to any available flat metal surface.

The use of an emitter resistor in the output stage results in some loss of power and sensitivity, although there is an improvement in the fidelity at moderate power levels. The revised performance figures are as follows:—

Editorial Note.—Looking at the output circuit, we see that, with the original output transformer and load, the collector load on each transistor is the sum of the following.

Emitter Resistor	0.4 ohms
Load Impedance reflected on half primary,	
Load Resist. + Sec. Resist.	
(Turns Ratio) ²	
= $\frac{4225 + 190}{335 \times 4}$	3.3 ohms
Resistance of half primary ..	0.25 ohm

Making a total Resist. Load 3.95 ohms

Allowing a knee voltage of 1 volt in the OC26, i.e. a peak collector swing of 11 volts, the peak current of the OC26 equals $11 \div 3.95$

Because of leakage inductance and iron loss the peak current induced into the secondary will be less than $2.8 \div 36.8$

And the power into the load will be less than—
 $0.077 \times 0.077 \times 4225$

12.5 w.

The iron loss is estimated at 0.25w, therefore if our calculations are correct it would seem that, with two perfectly matched transistors, one expects an output of just over 12 watts, and further, that in order to obtain 15 watts of audio power into the modulated stage, it would be necessary to obtain a more efficient modulation transformer and either—

- (a) Re-design the modulation transformer so that the primary impedance is 10 ohms, i.e. 52 turns per side.
- (b) Reduce the impedance of the modulated stage to 3,160 ohms, or
- (c) Increase the supply voltage to 13.5 volts.

We feel that taking normal variations of components into account, that the modulator would fall more happily into the 10 watt rather than the 15 watt class. We also feel that 0.9 of a volt is quite a bit too much to expect from average microphones, and a preamplifier stage would be necessary, and this, of course, entails a re-design of the input transformer.

COMPUTER "PREVENTS" SHIP COLLISIONS

A computer designed to act as the "eyes and ears" of sea-going vessels and which may virtually eliminate ship collisions, has been developed in the United States.

Designed to tie in with a ship's standard radar system, the marine collision avoidance computer was developed by the Goodyear Aircraft Corporation, Akron, Ohio.

A Goodyear spokesman said that the computer would give audible and visual warnings of collision courses, forecasting both relative and true courses of other ships 30 minutes in advance. In addition, the equipment advises the navigator of the necessary evasive action to manoeuvre out of a potentially dangerous location.

With existing ship radar, such information could be obtained only by plotting data obtained from the radar screen on a manoeuvring board, the spokesman said. Use of the computer provides continuous and accurate information without inebrious plotting, thus freeing the navigator and other officers for other important duties on the bridge.

Targets are automatically released from the trackers as they leave the 20-mile range, or may be manually released by the operator, the Goodyear spokesman added.

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DIVERSITY FOR THE AMATEUR

N. BURTON,* BERS-11494

THE Amateur Radio Service, in common with other Services using the short wave spectrum, has been, and still is, plagued with what is perhaps the most annoying of radio troubles—fading. Other Services have tackled this problem seriously, but apart from automatic gain control, which is only a partial palliative at the best, the Amateur has been notably backward in adopting any form of remedy against this nuisance.

Before the last war at least one commercial firm offered a diversity receiver for Amateur use, but in spite of the modest price, around £180, few Amateurs availed themselves of the benefits this receiver could offer.

The idea of diversity, as is well known, is to utilise the better of at least two signal voltages derived from separate aerials at any one instant, since, at any one instant, the voltages produced in different aerials by the same transmitter will vary widely.

A method was offered some years ago to Amateurs utilising the receiver a.g.c. line to operate a mechanical switch, but as the switching action depended on the uncertainty of a gas triode to trigger the switch, it, if for no other reason than this, failed to gain popularity.

The position today remains the same; fading is still with us and any Amateur today wishing to purchase a diversity receiver will find that the ones available commercially are meant for point to point w.t. or r.t. working and hence are ill adapted to rapid searching of the band. Even if they were suitable for rapid searching, the cost (around £1,500) is such that most Amateurs would give a second thought to the matter before purchasing one.

What can we do about the matter then? The answer would seem to be simple and within the means of any Amateur. It is to make our own switching device, but instead of using a

and, dependent upon the cycle, this applied voltage either adds to the standing bias on the valve, so cutting it off else it subtracts from the standing bias, and so allows the valve to conduct. The reverse cycle reverses the operation of the valves and so at any one instant only one aerial is connected to the receiver, but as this changeover occurs 30 times a second, it is rapid enough to provide a much more level audio output from the receiver and renders signals far more pleasant to read and so adds enjoyment to a contact.

Concluding on a practical note, it is suggested that the oscillator be well screened; also the filter components up to the output ends of the two rectifiers, whilst arranging the bias on the r.f. valves at cut off point, or almost so, it can be ensured that the valves do cut off or conduct. As little amplification is needed from these valves, there is no objection to a high standing bias on them.

NEW W.I.A. QSL BUREAU ADDRESS

Members are asked to note the new address for the Wireless Institute of Australia Federal QSL Bureau. It is also requested that VK stations, when in contact with DX stations, inform them of the new address so that the widest publicity can be given to this matter.

The following address should be used forthwith for all QSL Bureau business only:—

W.I.A. FEDERAL QSL BUREAU,
P.O. BOX 41, BOX HILL, E.11,
VICTORIA, AUSTRALIA.

FREQUENCY PREDICTION CHARTS

The Frequency Prediction Charts were discontinued due to space demands and the fact that it was considered they were of little interest. These Charts will be re-introduced as soon as suitable data is again available to "A.R."

The Publications Committee requests readers interested in these Charts to advise how they would like the data presented. Regrettably, cost prohibits their presentation in graphical form.

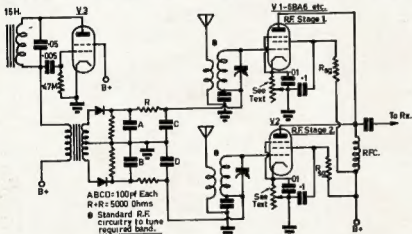
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The aerials may be spaced to obtain the largest voltage difference or they may be of different polarisation, which will produce the same effect, and this latter is perhaps the easiest for the Amateur, and technically for him, the best, since most short wave transmissions suffer varying degrees of rotation of polarisation in the reflections they make on their journey from the far point. It follows then that one aerial can be the normal transmitting aerial whilst the other aerial can be a simple dipole arranged vertically.

It is of course impossible to combine the outputs directly due to the phase difference, but some kind of switching from one aerial to the other allows the better signal to be used at any one instant. The switching could, of course, be done by hand when, aurally, the signal began to fall, but this method is hardly practical and is hardly in keeping with good practice.

clumy mechanical switch, to do the job elegantly, automatically and electronically.

Referring to the circuit, it will be seen that two aerials have been fed into separate r.f. amplifier valves and that these r.f. amplifiers share a common anode load and output condenser. This departs little from normal practice with the exception of the common anode load and this will explain itself as we proceed. The remaining valve is the odd man out. Close examination reveals this to be an oscillator of very low frequency—the values indicated set this frequency around 30 c.p.s. The output from this oscillator is fed via a Class B transformer into a pair of suitable small metal rectifiers at whose output, across the load resistors, appears a voltage which, after smoothing is applied, as would be a.v.c. to the grids of the two r.f. amplifiers.

The working is as follows: At any one instant one of the rectifiers applies a voltage to the grid of one of the valves

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75-WATT MODULATOR

THE modulator circuit is based on information appearing originally in R.C.A. "Ham Tips," re-printed in "Amateur Radio" (August 1948 and August 1960) and "Radiotronics" (July-August 1949) showing a method of using 807 valves as zero bias Class B Modulators. Tests have proved that this system produces the results claimed and does this without the usual complications of bias and screen voltages, etc.

Considering the popularity and low price of 807 valves, this circuit has much to commend it.

A complete modulator unit with pre-amplifier was designed, built and tested as a prototype, and all relevant tests were made including actual operation with a 100 watt transmitter. The performance of the modulator was very satisfactory, after one or two modifications were made to the original circuit in order to produce the required frequency response. The pre-amplifier provides sufficient gain for most high impedance type microphones.

● By popular request the following two articles are reprinted as the back issues of "A.R." are no longer available.

Many Amateurs are at a loss to know the best manner to obtain the audio power required to modulate their transmitters. A very good means to obtain 75 watts of audio is the use of 807s (or 1625s) in Class B zero bias.

TEST RESULTS

The frequency response was taken overall from the input of the driver valve to the secondary of the modulation transformer, terminated in a resistive load of 10,000 ohms, and with 100 mA. d.c. through the secondary winding.

At full output of 75 watts the frequency response was within 1.5 db. from 200 to 7,000 c.p.s. The distortion present at full output over the frequency range was quite low and aural tests

showed that the speech quality was excellent.

The response of the pre-amplifier stages can be modified to suit a particular microphone by altering the coupling condenser values and in the case of a crystal microphone by reducing the resistor value from grid to earth on the first valve. It will be noted that the low frequency response falls off below 200 c.p.s., the transformers being designed to aid in this respect.

Reduction of the high frequency response and harmonics produced by the negative peak clipping valve is also desirable, and can be achieved by the use of a filter or to a degree by a suitable by-pass condenser.

It is well known that speech waveform is of a very peaky nature, and this means generally that either a low average modulation level must be tolerated, or some means must be provided to overcome this limitation. Without suitable precautions, an increase of the audio gain above a certain level will cause some of the higher negative voltage peaks at the modulation transformer secondary to exceed the final

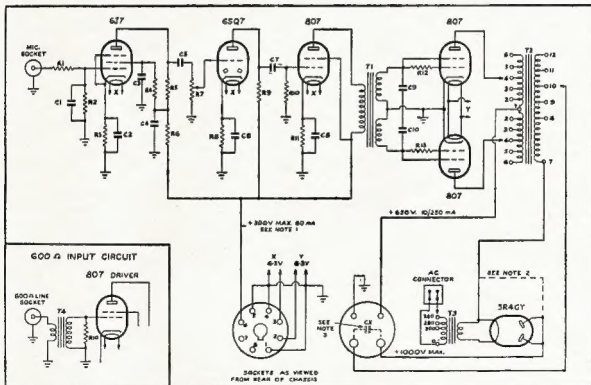


Fig. 1—Circuit of 75 Watt Modulator.

T1—Type IT588 A. & R. Transformer.
T2—Type MT15A " "
T3—Type PT1516 " "
T4—600 ohm input transformer.
C1—20 pF. mica.
C2, C3, C4—10 pF. 40 v.p.
C5—1 pF. 200 v.w.
C6—8 pF. 525 v.p.

C5, C7—0.01 pF. mica.
C8, C10—400 pF. mica.
C9—2,000 volt working, see text.
R1—20,000 ohms, 1/2 w.
R2—5 megohms, 1/2 w.
R3—1,500 ohms, 1/2 w.
R4—1.5 megohm, 1/2 w.
R5—0.25 megohm, 1/2 w.

R6—50,000 ohms, 1/2 w.
R7—5.0 megohm pot.
R8—5,000 ohms, 1 w.
R9—0.25 megohm, 1 w.
R10—0.5 megohm, 1/2 w.
R11—225 ohms, 3 w.
R12, R13—20,000 ohms, 1 w.

NOTES

1. If voltage exceeds 300, reduce with a resistor and by-pass with 8 pF. condenser.
2. Short circuit plates to filament if negative peak clipper is not required.
3. Up to 0.01 pF. by-pass may be required (inc. r.f. by-pass).

r.f. stage d.c. plate voltage. This will reduce the effective voltage acting on the r.f. stage to zero for the period of time that there is no positive voltage applied, thus causing discontinuity of the carrier power and so-called splatter takes place.

Volume compression and a.m.c. circuits reduce the peaks and increase the average modulation, but the time constants normally used allow high speed speech peaks of some frequencies to pass through to the modulator output circuit. The solution to this is to add a high level negative peak clipping valve with a low pass filter following.

The negative peak clipping circuit is included in the modulator so that those who use the equipment will be provided with the basis for possible improvement of their transmissions if they desire a high average modulation level with minimum interference to other stations.

It is not claimed that the best results will be possible without a low pass filter between the modulation transformer and the r.f. final stage of the transmitter, although useful suppression of high frequency response can be obtained by providing as large a capacitance as possible (2,000 v.v.) in the position marked CX in the circuit.

A filter, if used, will carry the final stage d.c. current and the audio frequency currents. The condensers and reactors should be able to withstand the maximum working voltage continuously; i.e., approximately 2,000 volts r.m.s. at full audio output and 1,000 volts d.c. It is best to use "air core" reactors for the reason that less trouble will be experienced from noisy operation under heavy modulation.

Details of the design and operation of suitable filters, and of other methods of reducing the i.f. channel width will be found in "QST," April 1948; R.S.G.B. Bulletin, February 1949, and in other publications.

VALVE LINE-UP

The modulator includes pre-amplifier stages, and is intended for use with a high impedance microphone. The overall gain is more than sufficient for full output using a D104 type crystal microphone.

A 6J7 metal valve was used in the original unit, and should this type be difficult to obtain, a 6J7G would be quite suitable if provided with a metal shield to completely enclose the valve,

grid resistor and r.f. filter circuit. A single ended valve, such as a 6SJ7 is not recommended.

The second valve is a high gain triode type 6SQ7, and this valve and the following valves are readily obtainable.

It was found that a single 807 valve as a tetrode provided adequate driving power for the modulator valve, when used as shown in the circuit diagram. Negative feedback was not necessary, as the distortion visible on the c.r.o. screen was not excessive at 75 watts output, over the voice frequency range for which the unit was designed.

The driver transformer is a type specially designed for use in this circuit, but the modulation transformer is a semi-universal type suitable for use with many other Class A, AB1, AB2, or B circuits, using such valves as 807s, 809s, 830Bs, etc. The maximum signal modulator valve plate current should not exceed 150 mA. d.c. per side of c.t. on the primary side, and the d.c. current through the secondary should not exceed 150 mA. A maximum d.c. voltage of 1,000 may be applied to the primary and/or secondary windings.

MODULATION TRANSFORMER IMPEDANCES

PRIMARY	SECONDARY
1 H.T.+	7-8 4,000 ohms
2-2 3,800 ohms	7-9 5,000 "
3-3 5,000 "	7-10 6,000 "
4-4 6,800 "	7-11 8,000 "
5-5 8,500 "	7-12 10,000 "
6-6 10,000 "	

The modulation transformer is fitted with a spark gap to provide protection against excessive peak voltages which may occur in the event of loss or reduction of load during transmitter adjustment or tuning operations. This gap should be carefully adjusted so that during full modulation the points are as close as possible, but do not spark over under normal peaks.

The modulation transformer has been carefully designed and is not likely to break down with normal use if the maximum voltage and current ratings are not exceeded. The primary and secondary impedance ranges should be suitable for most modulator and transmitter valve combinations usual with a transformer of 75 watts rating.

POWER SUPPLY

It is necessary now to point out that full power output with low distortion from this or similar audio equipment, is not possible without power supplies having the necessary voltage regulation under minimum to maximum signal conditions.

The power supply for the pre-amplifier and driver stages should provide 275/300 volts at about 80 mA. with sufficient filament windings for all valves (except the 5R4GY). It is advisable to check the filament voltages at the valve sockets, as low voltage, particularly on 807 valves, is to be avoided.

The power supply for the modulator valves is most important, and should be a separate unit with good regulation. The voltage output should be approximately 650 volts at the no signal current of 10 mA. and should not drop to less than about 600 volts if full output of 75 watts is required, the maximum signal current for both valves being approximately 220 mA. It is possible to use up to 750 volts (maximum at no signal) on the valves, and obtain the power output with poorer power supply regulation. A power supply with good regulation and additional current capacity may also be used for both the modulator valves and the Class C final r.f. amplifier.

The degree of voltage regulation required can be obtained by using 868A rectifier valves, with a choke input filter (preferably a swinging choke) and a second filter choke, both with low d.c. resistance of the order of 50-60 ohms. The filter condensers may be 2 μ F. after the first choke and 4 μ F. after the second choke.

When wiring the modulator, make all earth connections to a bus-bar, and earth at one point only on the chassis.

MODERNISING THE DRIVING STAGES

The 6SQ7 can be replaced by a 6AV6 or one section of a 12AX7, and the 6J7 by a 6BR7 or EF86 or similar low noise pentode.

Alternatively, the 6J7 and 6SQ7 can be replaced by a 12AX7 with both sections in cascade if the microphone has sufficient output.

Fig. 2 is from the S.T.C. Valve Data Handbook, Vol. 2. It is necessary to use separate cathode bias resistors and condensers and suitable plate decoupling. Plate and grid leads should be kept short and separated with shielding if required. For voice frequencies, the cathode and coupling condensers can be reduced in value to limit low and high frequency response.

★

Fig. 2.—12AX7 Cascade Amplifier.

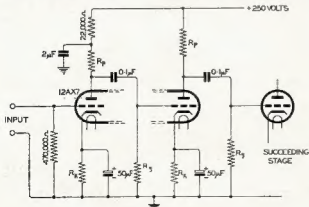


Plate Load Resistance R _p (ohms)	100,000	100,000	200,000	200,000	470,000	470,000
Grid Leak Resistor R _g (ohms)	220,000	470,000	470,000	1M	1M	2.5M
Cathode Bias Resistor R _k (ohms)	1,500	1,500	3,300	3,300	6,800	6,800
Max. r.m.s. output voltage at 1 kc. for 5% total har- monic distortion	27	31	35	33	26	32
Voltage gain at 1 kc.	2,080	2,420	2,940	3,370	3,420	3,590

DRIVING THE ZERO BIAS 807s

NOWADAYS it is quite common to hear "I am using 807s in zero bias as modulators" OM," and find another convert to using our "Maid of all work," the 807, in a new job.

This is quite understandable, for used in zero bias, the 807 is completely tamed, and parasites are non-existent. For those who have not got access to the original article, it may be as well to run briefly over the circuit, shown at "A" in Fig. 1.

The centre tap of the driver transformer is grounded, and the ends of the secondary windings connected to the screens of the 807s. A 20,000 ohm resistor is connected between the screen and grid as shown, and the plates of the 807s are fed to the conventional modulation transformer. The cathodes of both 807s are grounded.

With this circuit, the driver transformer was the catch, as it had to match the driver tube to the grids of the 807s which had an almost constant impedance of 14,200 ohms, grid to grid. In addition, to obtain 120 watts of audio it was necessary to use a driver which would supply 5 watts of drive to the grids; this meant a pair of 2A3s or equivalent, after allowing for transformer losses, etc.

In our applications, 120 watts is not required, and therefore the most popular arrangement has been to use a 6L6G as driver, which allows us to obtain at least 75 watts of audio, and for lower audio requirements, a 6V8 or 6V6 was adequate. Obviously then, with zero bias 807s, the harder we drive them, the more we get out, up to their limit of 120 watts, provided of course, that our plate voltage, regulation, and impedance match are correct.

Ahead of the driver, we need the usual voltage stages to lift the gain from the microphone to give a voltage which will enable the driver to operate at its correct output. With a crystal microphone, this is about two stages, or with a carbon microphone, one stage.

So much for the circuit as originally described, and now to the circuit described in February 1950 "CQ," shown in "B" Fig.

T1 is a conventional plate-to-push-pull input transformer, such as the type used to feed a 6C5 to a pair of 2A3s; in other words, an ordinary voltage transformer (most of us have a transformer of this type lying about). The centre tap of the transformer is grounded, and the ends of the secondary fed to the grids of a 6SN7, which operates as two cathode followers. The cathodes are not grounded, but are connected as shown to the 807 screens and grids.

The plates of the cathode followers are tied together, by-passed, and supplied with 300 volts. The remainder of the circuit is the same as "A."

Conventional methods of producing driving power in circuit "A" Fig. 1 would involve power consumption largely cancelling the power economy advantages of the Class B operation. Such power need be supplied to each grid only on its positive half of the cycle, however, the cathode follower driver is a natural.

Note there is no connection from the 6SN7 cathodes to ground, except through the grids and screens of the 807s. Thus the plate current flowing in the 6SN7 is equal to the grid and screen current of the 807s, and varies from less than 1 mA. to peaks of 20 mA. with voice modulation. Actually the total current of a 6SJ7 pre-amplifier, 6SN7 two-stage resistance coupled triode amplifier, and the 6SN7 cathode follower stage totals less than 10 mA. under static conditions. Since the driver section works on about 250 volts, its plate power as well as that of the two voltage stages is obtained from the one supply.

Actually the direct-coupled cathode followers supply approximately 10 volts of positive bias with resultant total static plate current on the 807s of 30 mA. Of course with modulation, this plate current increases to 80 to 150 mA., depending on the output required.

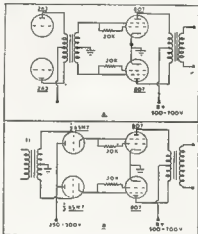


Fig. 1.

The voltage stages required ahead of T1 are important, and it is necessary to see that sufficient voltage is supplied to the primary of T1, otherwise the power output from the 807 stage will be inadequate.

It is recommended that the minimum required from a crystal microphone would be: a 6SJ7 high gain amplifier, followed by two triode sections of a 6SN7 as resistance coupled triodes. In the writer's case the voltage stages used were:—

Pre-amplifier on operating tube, 6SJ7 and 6J5 to 500 ohm line, 6SN7 as two resistance coupled amplifiers, feeding T1, cathode followers and then the 807s Class B stage. From the 500 ohm line, all other stages are in the main rack of the transmitter. With this line-up, the gain control is one-fourth on for 100% plate modulation of a 50 watt power amplifier, i.e. 25 watts of audio. The meter reading the combined plate currents of the 807s varies from a resting current of 30 mA. to about 80 mA. on peaks, which means that for 25 watts of audio, the 807s are simply loafing along. The plate to plate im-

pedance was 10,200 ohms, and the plate voltage 500 volts, rather poorly regulated.

IMPEDANCE OF CLASS B STAGE

The following plate-to-plate impedances for the 807 Class B stage are appended for readers who have not a copy of the original article.

Case	1	2
Plate Volts	750	600
Plate to Plate load	6850	5050
Output	120	90
Max. av. anode current (two valves)	240	240
	240	240

Note.—If the Class B stage is run at lower plate currents or voltages, the plate to plate impedance will be different. The calculations are very simple with the following method, which is accurate enough for our requirements.

CALCULATING IMPEDANCE

In a Class B stage at any instant the grid of one tube will be driven positive and the other tube driven past cut off, and therefore in calculating impedances we need only consider one tube. As far as the one tube is concerned the primary of the output transformer is a resistance and therefore we have this plate load (R_p) and the resistance of the Class B tube in series across the power supply. We can assume that about 80% of the power supply voltage will appear across the plate load R_p , as audio voltage, so if our plate supply is 500 volts, 400 volts peak of audio will appear across the plate load R_p . This gives us our voltage for calculation.

Now we want the peak current. Manufacturers' characteristics give the maximum average current for two tubes (sine wave input), so to find the peak current we divide the average current by 0.636. Therefore our peak current for Case 3 in the lists above is: 240 mA. \div 0.636 = 377 mA. = 0.377 Amp.

Then from $R = E \div I$ we have: $400 \div 0.377 = 1061$ ohms for one tube.

The plate to plate load for two tubes will be four times this value or 4244 ohms, which is very close to the manufacturers' ratings (Case 3).

The audio output can be found by the simple formula $W = (I \times E) \div 2$ and working on peak values found, we have $(0.377 \times 400) \div 2 = 75$ watts output.

Below is the case of Class B 807s to give 100% modulation of a 50 watt carrier (25 watts of audio). Example: Supply voltage 500 volts.

Av. I_p (2 tubes) = 100 mA. = 0.1 Amp.
Then $E_{peak} = (500 \div 1) \times (80 \div 100) = 400$ volts.

(i.e. 80% of supply voltage.)

Peak current $I_p = 0.1 \div 0.636 = 0.152$ Amp.

Plate impedance (one tube) = $E_p \div I_p = 400 \div 0.152 = 2630$ ohms.

Then plate-to-plate impedance = $2630 \times 4 = 10,520$ ohms, and audio output = $(I_p \times E_p) \div 2 = (0.152 \times 400) \div 2 = 30.4$ watts.

—J. C. Duncan, VK3VZ



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CALCULATING INPUT IMPEDANCE OF GROUNDED GRID LINEAR AMPLIFIERS*

JOHN WEATHERLEY,† VK5QL

Impedance matching in grounded grid linear amplifiers seems to be a problem worrying many Amateurs. The following notes are based on articles published over the past few years in British and U.S. magazines. The notes refer to tetrodes and pentodes connected as high-mu triodes as these are probably the types for which this type of information is difficult to obtain.

In a g.g. amplifier there are the same number of impedances to be matched as in a normal grounded cathode amplifier. Impedance matching is probably of greater importance in a g.g. stage because the input and output impedances appear in parallel to the driver stage (see Fig. 1).

It will be seen that any variation of either parameter will affect the other; this can demand high drive. The actual basic circuit with impedances indicated is shown in Fig. 2.

The plate load impedance Z_L is calculated the same as for any power amplifier. The input impedance is a different matter and apart from being complicated, requires tube data not normally available. Fortunately a simple approximation can be made for the input impedance of g.g. tubes connected as high-mu triodes.

First the conductance is calculated—this is the opposite of impedance. If the plate resistance R_p is much greater than the load impedance Z_L and the μ of the valve remains much greater than unity, the input conductance g_i can be shown as

$$g_i = \mu + R_p = g_m$$

where g_m is in umhos,
 R_p is in megohms,
 μ = amplification factor.

This represents the tube conductance in g.g. As impedance is the reciprocal of conductance the input impedance Z_i may be determined by dividing the g_m into 1 (one). The tube transconductance can be readily obtained from tube tables and if this is in turn divided into 1 (one) will give the input impedance Z_i in ohms.



Fig. 1.

For example, the 813 has a transconductance of 3,750 micromhos, the formula becomes $10^6 \div 3750$, which becomes 267 ohms or the impedance to which the driver must be matched to give maximum transfer of power.

It should be remembered that tubes in parallel will behave the same as resistors in parallel and two 813s in parallel would thus have an input impedance of 133.5 ohms.

Table 1 lists some of the tubes found to perform well with both control and

screen grids grounded and in the case of pentodes with separate suppressor with this grounded also. The transconductance was obtained from manufacturers' data sheets and input impedance from the formula $Z_i = 1 \div g_m$, where g_m = transconductance in mhos.

Valve	g_m umhos	Input Z_i ohms
6AG7	11,000	91
6V6	3,750	267
6L6	5,200	192
802	2,250	444
837	3,400	294
6146	7,000	143
4E27	2,800	357
4E27A	2,150	466
4-125A	2,450	408
813	3,750	267
803	4,000	250
4-250A	4,000	250
1625 (807)	6,000	167
EL34	11,000	91
EL38	11,000	91
4X150A	12,000	83

Table 1.

[The above g_m only apply at a specific series of voltages.—Ed.]

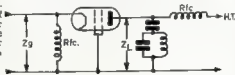


Fig. 2.

Trade Review

V.T.V.M., MODEL 300H

The new v.t.v.m. model 300H by Ballantine Laboratories, Bonton, N.J., U.S.A., is capable of measuring voltages as low as 30 microvolts and as high as 300 volts over a frequency band of 10 c.p.s. to 1 Mc.



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Full technical information is available from Warburton Franks offices in Queensland, New South Wales, Victoria, South Australia, and in Western Australia from Tough Instrument Service Co.

"AN AWARD OWED"

Conditions these days, are not very good And QSLs aren't returned, as I think they should

At times I hear prefixes from all over the place,

And so do others who get in the race. It's very enjoyable to work a rare station And receive a card without much frustration

But sometimes I find it extremely hard To persuade a station to send me a card. And as for Certificates, I seem to recall That I've won a couple, but they're not on my wall.

Is it procrastination, or writer's gout, That prevents 'em from sending them out?

I'm referring, of course, to the R.D. Award

And their reluctance to send one to Claud.

I have heard just lately of tidings dire, That these awards and records went up in a fire.

It must have been serious, of that I've no doubt,

'Cos it's taken a year to put fire out. In the meantime, of course, the contest continues.

But how can you win? They're all again yours.

The whole complete set-up has a certain aroma,

Why in heck won't they issue an R.D. diploma

To those willing log chasers who worked night and day?

I "dips me lid", they're not in the fray. But that elusive character, the award designer,

Where in heck is he, on a slow boat from China?

In a recent "A.R." some mention was made

That the necessary blocks didn't quite make the grade.

"Get on it" chaps, their excuses are worn,

Why try to hand us "a very raw prawn".

The contest itself has meaningful aims To remember our comrades, to treasure their names.

In conclusion, may I have this to say, If you can't do the job, you'd best give it away.

—C. P. Singleton, VK4UX.

* Reprinted from S.A. Division, W.I.A., Bulletin, 110 Green Street, Elizabeth Park, South Aus.

SPACE COMMUNICATIONS IN AUSTRALIA

Australian Amateurs lead the world in reporting of Oscar 2! Congratulations, chaps.

Oscar 2 is dead, though its memory is still with some of us, but Oscar 2 is known by many more of the VK boys. We watched its progress, measuring its temperature, its speed, its height, placing a protractor along the equator and knowing the inclination to be 72 degrees at the equator, produced the orbital path across our continent with a few figures, and the knowledge that the earth moves from west to east at 15 degrees each hour (at the equator), worked out the number of degrees per hour we move here at Sydney. (For those interested, it is 40 naut. miles per degree.)

Thus after having worked out the number of orbits per 24 hours (60° times 24 hours/90° = 16 per day) we were able to make our own predictions as to when and where Oscar would be at any given time. All States had their own Co-ordinators who were supplied with full data on how to find Oscar, Doppler shift, slant angle, and so on.

We ran a Oscar 2 network on 3.565 Mc, where you could hear what was going on daily. The operators of this net were VK3ABP (Bill), VK7PF (Peter), VK2WH (Hugo) and VK2HO (Roy). We tried the 40 mx band, but it was a wash out. I also tried out 21 Mc, but it was too inconsistent.

At headquarters here in Sydney, phone calls, letters, telegrams and visitors were frequent daily. Much information had to be sent across the continent each day, not to mention the report form service. The W.I.A. N.S.W. Division were busy printing the forms, and also printed a special sheet on how to find Oscar 2, etc., thanks to Tim VK2ZTM and Tony Patterson. In N.S.W. there were small country groups

under selected leaders, and they were the Lismore group, Woolongong, Blue Mountains, Tumut, Kullnura, Gosford, Canberra and s.w.I's. all over the State. Single operators in country towns did a very good job, not forgetting the many v.h.f. groups in all the capital cities.

VK2ZCF ran a tape on 144 Mc., a recording of Oscar 1, and from this all were able to get some idea what to look for, and what the Doppler shift sounds like, how to count the H's, etc. This proved very useful. VK2ZJC, at Kurrangong, did a sterling job and logged the greatest number of fly-overs in his State, giving times, H1 rate, and predictions. Publicity was given to the project via t.v., radio stations, newspapers, magazines, bulletins, etc.

Reports are flowing into Oscar headquarters from all parts of the world. Special honors are due to the Amateurs of Australia, Finland, Austria and England who are providing a great volume of excellent data. Reports from all call areas in W land are excellent. Ed Hilton, W6VKP, states that Oscar 2 reports show a much higher degree of competence and awareness than did the reports received from Oscar 1. Obviously the self-training aspect of Amateur Radio is working well! Many Amateurs are computing Doppler curves, determining satellite slant range, and figuring the period of the satellite and making their own orbital predictions. Congratulations!

To date, 428 stations have reported data to headquarters, with more mail arriving every day. Most reports are of such excellence to enable the Data Reduction Group to directly transcribe them to I.B.M. punch cards for quick sorting and analysis. This operation is now in progress under the direction of Harley Gabrielson, W6HEK. Early analysis indicates satellite temperature remained relatively constant, rising slowly from a lunch figure of 20°C. to

30°C. by revolution No. 293. By revolution No. 294 the package temperature was up to 44°C. and by revolution No. 295 the temperature had soared to 58°C., which is close to the temperature of transistor failure.

Headquarters in America send their congratulations to Amateurs in Australia. Through your efforts the number of reports from VK (based upon Amateur population) are first compared to all countries, and they are excellent in quality. One of the Oscar crew works at I.B.M. and all Oscar 2 data is being placed on punched cards to run through a computer. This will greatly aid the analysis of data. Headquarters staff offer their profound thanks to the VK gang. "It is a pleasure to obtain such co-operation, which stresses once again the International friendship and co-operation that exists within the ranks of Amateur Radio! I am sure that the long-range effects of the Oscar programme will be of great benefit to our hobby."

In conclusion, I wish to thank all who participated in this project. I want to particularly thank all State Co-ordinators, VK1ML, VK3ABP, VK7PF, VK2WH, VK4ZBT, VK5ZX, VK6ZDS, and VK8AU for a very excellent job indeed.

Further, I thank VK2HZ, VK2PF for publicity. Last, but not least, the Council of the W.I.A., N.S.W. Division, for co-operation.

Chaps, don't stop now! Oscar 3 is on the way, and let us be on top again in this next project. Oscar 3 will be a communications satellite not unlike Telstar.

Cheers and 73,

—Roy Hart, VK2HO,
Australian Co-ordinator.

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FILTERS

Editor "A.R." Dear Sir,

In his article on "The Importance of Adjacent Channel Selectivity" (August "A.R.") Ed Mr. E. C. Hulme, VK2EN, inferred, possibly unintentionally, that crystal filters are inferior to mechanical filters. I would like to make the following points:

1. It is just as impractical for the average Amateur to construct a mechanical filter as it is for him to build a modern crystal filter. No Amateur, to my knowledge, has attempted to manufacture a mechanical unit and the reasons for this are illustrated by VK2EN's comments on the "work" of such devices. Those crystal units described in constructional articles cannot be considered as representative of modern filter units as they invariably use obsolete types of crystals. A modern crystal filter uses hermetically sealed, plated crystals carefully manufactured for frequency, inductance and lack of spurious responses. The average Amateur just has not the facilities available to make such crystals and thus he must purchase a "black box" to get a first class unit.

2. If the filter is considered as a "black box" supplied by a manufacturer then neither the mechanical nor crystal type of unit is particularly difficult to install provided the directions are followed.

3. Shape factors obtainable with mechanical filters are also possible with crystal filters, e.g. a six-crystal filter can be built with a shape factor of 3:1.

4. The insertion loss of a crystal filter is usually considerably less than that of a comparable mechanical unit, e.g. 5 db. as compared to 20 db. Figures on in-band ripple are of the same order, viz. 1 db.

5. Crystal filters can be made for frequencies between 50 kc and 40 Mc, whilst, at the moment, mechanical filters are limited to frequencies below 500 kc. This means that in receivers employing only one i.f. and a mechanical filter, the i.f. is of necessity low and image responses are still a problem. However, if the one i.f. is of the order of 5 Mc and a crystal filter is used, then good selectivity is obtained where it is most needed and images are no longer a problem.

6. In all fairness, however, I would point out that within the range 400-600 kc the mechanical filter is smaller and usually more economical than the crystal type.

Summing up, it seems the mechanical filter is the better proposition for the Amateur i.f. a.s.b. exciter but there is no doubt that the h.f. crystal filter is the device for the modern communications receiver whether it be for c.w., a.s.b. or a.m. work.

—David Rankin, VK3QV.



"A.R.'s" DX Editor, Al VK4SS

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SPLATTER

Editor "A.R." Dear Sir,

I would be the last to brand VK5PU's criticism of my article on "Splatter, Its Cause and Prevention" ("A.R." July '82) as hysterical.

No claim was made by me for originality in application of a shunt diode to provide a conductive path for excessive negative swing of modulation potentials; even the generation of ringing frequencies dependent on the distributed constants of open circuited inductors is a well known factor. However, the realisation that this phenomenon is the basic cause of monkey chatter heard during excessive modulation, and NOT audio frequency harmonics of the fundamental speech signals seems to have escaped attention.

The "Amateur Bible" (A.R.R.L. Handbook, p. 235, 1982 edition) persists in the erroneous explanation that splatter is due to audio frequency harmonics generated by clipping of the modulation envelope, consequently confusion among its devotees is explainable.

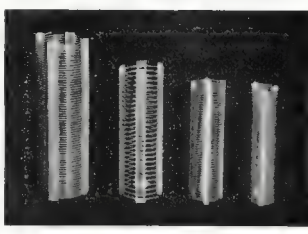
Permanent "Negative Cycle Loading" as advocated by Reinartz ("A.R." March '82) is a decidedly amateurish and brute force method, wasteful of audio power, and a chronic source of audio frequency distortion at all levels.

Low pass filters in the modulated amplifier h.t. supply undoubtedly assist in reduction of modulation by lower order audio harmonics of speech frequencies, and should be used in addition to any form of Negative Cycle Loading or clipping. At the radio frequencies generated by ringing of open-circuited modulation inductors the usually jumble wound filter coils no longer operate as essential inductances but by-pass increasing levels of splatter producing energies.

In conclusion, I would like to stress that my article was intended to place before the Amateur fraternity a simple method of serious splatter cure, not requiring specially wound and insulated diode heater transformers. Also to VK2AZG I would like to publicly express my appreciation for his assistance in making available the 6R5/6AL5 diodes.

—J. G. Reed, VK4JR

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2-16	1/16"	16	3"	No. 3007	6/3
3-08	3/8"	8	3"	No. 3010	7/4
3-16	3/16"	16	3"	No. 3011	7/4
4-08	1"	8	3"	No. 3014	8/5
4-16	1"	16	3"	No. 3015	8/5
5-08	1 1/8"	8	3"	No. 3018	10/6
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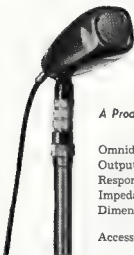
References: A.R.R.L. Handbook, 1981; "QST," March 1959; "Amateur Radio," December 1959

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NEW SOUTH WALES

At the V.h.f. Group committee meeting on 20/7/62 two members of the Group were co-opted to help out as Reg ZECK had resigned and also another committee member indicated that he may be leaving the State, although this was not finalised. The committee wishes to thank John ZAAW and Terry ZEBL for coming forward.

The Group meeting was held on 2/8/62 where the lecture was given by Barry Z2AG on a V.h.f. Mx. a1x1 locked converter. The Group meeting for Sept will be held on the 7th, as usual on the first Friday of each month.

The day event for Sept. will be a long distance fox hunt, held on Sunday, the 10th. I would like to be able to include v.h.f. news from areas other than Sydney as I understand v.h.f. activity is relatively high in other areas, such as W. Zoz, but unfortunately very little news filters through regularly. If anyone has any news they think would be suitable for inclusion would they please contact me on 144.12 Mc. or write to 17 McIveries St., Canley Heights, N.S.W.

144 Mc. Conditions have been reasonably good, seeing it is the middle of winter and the New Year holidays are being celebrated regularly. Unfortunately the converse does not apply, which is probably due to higher noise level, especially V.KS and not listening in the right spot at the right time.

Concurrently with the sporadic E opening on 30 Mc. many stations are listening for break through on 144 Mc. On 14/7/62 Ken ZRL reported hearing JARI (?) calling CQ at 1311 E.S.T. At 1321 E.S.T. Z2PO (?) was heard and Z2AD heard between 1220 and 1254. It is not been verified if these calls were active on the VKS and VKD calls was not clear. Horrie did suggest that the stations were heard on the transmission from 50 Mc., but this angle could not be confirmed.

New stations heard this month include Z2XB at Balgownie, Z2BC at Terry Hills, and Z2OK from Santa Souci, which was last heard on 2 m nine years ago but has made the plunge again.

Also ZAAK at Kilmurns and David Z2VW at Bays have been using E.S.T. with vox control for their CQs. Tony Z2BU of Wailarah has been discovering the joys of a tall locked converter.

Me. Openings occurred regularly each Sunday during the early part of July. One of the best openings occurred on 15th when State exper. VKS and 288 were audible at various times during the day.

30 Mc. No activity at the moment, but Z2AH/P and RHO have claimed a State record 742.5 miles from St. Ives to Mt. Gibraltar, V3, Z2LB.

VICTORIA

VKS Friendly Frequency.—If you have ever tuned up to 140.850 Mc. you might have heard some peculiar sounds. Probably you have tuned in a station operating in the fm. net. The net operates equipment that was available some twelve months ago through the Victorian Division's disposal department. The mobile net has been taken to 288, and the 288 rx's are double converted, and both are crystal controlled. The tx has a total of 10 tubes, the rx 14. Mobile to mobile contacts are common over 15 miles and on occasions up to 50 miles. Stations active include ZDP, ZEM, ZBK, ZNR, ZOM, ZIK, ZOM, ZAVE, ZARD, Z2CA, Z2GO, Z2GO, Z2GO, Z2GO. It is hoped that in the near future we will be able to publish details of a crystal co-mediator which will convert any 8 m. tx to the fm net frequency. So watch out for it. To, ZOM.

QUEENSLAND

Murrumbidgee bomb. July DX has never been so good. On 7th, 11th and 12th—VKKS; on 13th, VKS, 5, and 7; on 14th, VKS; on 15th, we had VKS, 5, 6, 7 and ZL land; on 16th, VKS and ZL; on 17th, ZL and 288; on 18th and 19th the band was open to VKS and 5. On 20th, to VKS; 22nd to VKS and VKS, and on 24th, to VKS.

On 24th it was just coincidence about the H bomb, but if we could have the opportunity to study further similar experiments it may be of value in understanding the modes of propagation at v.h.f. better.

New station on 6 mX is Ken Z2CP, who is running 6w. into a folded dipole nailed to the wall. Rx is a 658 converter into a con. rx. Other gear is owned by Ken and his XYL is a brand new baby daughter.

Reverend Doug Z2DL now visits Brisbane every Tuesday and it is a very great pleasure to hear his voice again after a long absence. Previous to this only the Gold Coast had the benefit of Doug's presence on 6 mX. George Z2GD is now in the wilds of Tully in North Qld. He points out that not only is there a great lack of enthusiastic and progressive Amateurs, but there are very few full licenses also.

Newcomer to this part of Brisbane is Bruce 4BZ and his family. Bruce has returned from the Toowoomba area at last. V.h.f. activity in this suburb, Mt. Gravatt, seems to be mysteriously growing. There are Amateurs, Amateurs moving in, Amateurs who are going to move in, and budding Amateurs. With such a concentrated area of v.h.f. we may eventually create a t.v. set-free zone or something.

The V.h.f. Group meeting was held on the third Friday of the month at the Social Services Institute Hall at Berwick Street, Valley. This is now the new time and place. The meeting was well attended, was organised, was noisy, in fact even some business was attended to, 73, Z2BT.



A guard of honour was formed at the recent wedding of Christine and John Z2Z (ex-ZCJ), ZTN and SBQ are holding the 2 mX yagis to form the arch. A very high percentage of the guests were V.h.f. Group members and notable amongst them were VKS Z2B, 3KIK, STN, Z2DN, Z2CQ, Z2DQ, Z2AR, Z2BI, SBQ and SND. Radio contact on 6 mX was maintained with the newly weds on the first leg of their honeymoon. (SBQ mobile to the bridegroom's car)

WESTERN AUSTRALIA

July Meeting: 30 members and visitors attended. Four new members were welcomed to the Group. These were Michael Z2CX, Ian Z2CLR, Trevor Z2DQ, and Graham Blynn who has sat for the L.A.O.C.P.

Cover Island Beacon Work is still continuing on the gear and antenna for the installation of this beacon. Further progress will be reported in next month's work.

V.h.f. Field Day Award: Entries received for this award following the field day were of a very high standard. It was found impossible after due consideration to separate the entries of John Z2AG, Vic 6VK and Dennis 6AW. The prize was divided and presented to these stations.

Western Video Transmitters Club, VK6WVT. This club has been transmitting regularly on 222 and good results have been achieved in reception using a converter into a V.h.f. V. set on Channel 3. Numerous reports have been received on picture quality and many have been made on the quality of the transmission times are: Week days, 1100-1400 hrs., 1900-2200 hrs.; week-ends, 1500-1900 hrs., 1900-2200 hrs. Test patterns and caption boards have been the main subjects, but technical transmissions are aimed at soon.

V.h.f. Group Annual Meeting: The minutes of the previous annual general meeting were read. Wally Z2AA read his report as the repre-

sented President. He reported on the achievements and successes of the Group during the preceding year. He thanked the Secretary and members of Council for their support, and also thanked all members of the Group for their support in running the Group and participation in the Group's activities and contests.

The election of officers followed. Those were Patron, Mr. Graham; President, Wally Z2AA, Sec.-Treas., Rod Z2DS, Council: Den 6HK, Dennis 6AW, Kevin 6ZCB, Trustees: Ken 6FM, Syd 6SL, Aliaks: Mr. Dooley, John Z2AG, Press Correspondent, Alvin Z2DM, Programme Directors: Max 6MM, Dennis 6AW; Contest Organiser, Lance 6LR; Keeper of the Records, Charlie 6LK, Librarian, Reio 6BO; QSL Manager, Lance 6LR.

An award was founded for the most outstanding achievement in the field of v.h.f. Amateur Radio by a member of the V.h.f. Group. This award will be accompanied by a remuneration of £5/5/0 as an incentive for amateurs to further the achievement and technical ability of Amateur Radio in general.

30 Mc. The first major v.h.f. opening during winter was experienced here on 18th July, V3, 2, 5, 6, 7 and 288 were heard and worked. The band was open from 0800 hrs. to approx. 1400 hrs. W.A.S.T. Conditions were so good that both Z2DW and Z2DC reported hearing ZAXI mobile, but were unable to make contact with him. Except for the activity this break through caused, 50 Mc. has been fairly quiet. Ian Z2CP has been heard and worked on the double sideband. Peter Z2BK has a tx working and is now working on a converter and beacon.

44 Mc. Bob Z2DP has just completed a converter for this band and both he and Brian Z2DE are building 10 el. yagis. Viv Z2CM is hoping to be on the band soon. As usual cross band operation to 50 Mc. is the major activity on this band.

50 Mc. Major activity is building of converters to receive the Amateur t.v. transmissions by 8WV/T.

It has been seen in the past that winter time is building time so it is this year a number of mobile stations have appeared on 50 Mc. this month, talk of 144 Mc. mobile has been heard in a few quarters. The opportunity was taken for modification of existing equipment by both Z2BV and 8AU and both stations were inactive during the month. At the time of writing Z2BV still has to replace his converter slot socket and 8AU has to carry out a lot of wiring on a new converter for 30 Mc. Murray Z2CK had not made any alterations and is active again on 5 mX, but he hasn't heard anything other than some 49 Mc. TX signals from our friends up north.

No activity at all during the month on 144 Mc. 73, 8AU.

PAPUA

What confusion regarding frequencies available for use! We were amongst those caught and were not aware until the last few days of July that 50-52 Mc. was in fact still available for use in Queensland. The opportunity was taken for modification of existing equipment by both Z2BV and 8AU and both stations were inactive during the month. At the time of writing Z2BV still has to replace his converter slot socket and 8AU has to carry out a lot of wiring on a new converter for 30 Mc. Murray Z2CK had not made any alterations and is active again on 5 mX, but he hasn't heard anything other than some 49 Mc. TX signals from our friends up north.

No activity at all during the month on 144 Mc. 73, 8AU.

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Sub Editor: ROBERT YOUNG, WIA-L3076,

14 Alverna Grove, Brighton, Victoria

ADDRESS CORRESPONDENCE FOR THIS PAGE DIRECT TO THE SUB EDITOR

Here we are once again with information on activities of the s.w.l.s in Australia. Firstly, I must apologise for the absence of news in the August issue of "A.R.". The reason was that only two letters were received by me for the notes. As you can understand it is impossible to write a page of notes out of practically nothing. I wish to thank the few regular members for their support every month. So chaps, how about helping to support this page by writing of your activities or equipment, etc?

VICTORIA

At the last general meeting of the group, 19 members were in attendance. The meeting moved very smoothly, but nothing happened of great interest. After the closing of the general meeting we were all shown how VK3-SWI operates on 6 and 3 mcs. We contacted a large number of Amateurs while on the air.

At the construction night on 14th Sept. Ian 12000 will supply a parts list and circuit for those who intend building a 30 Mc converter. It will be a three-tube unit with an L/C osc. and will feed into a tunable i.f. in the s.w. range. It will require a power source of 63v. and 100 to 250v. h.t. The finished article will also be at the meeting. Those who intend to construct this should bring along a list of all the glass-base valves they have, pentodes, twin triodes and triodes being most useful. We will advise you.

A large group turned up at the visit to VK3APC it had been decided to continue the visits to places of interest for the rest of the year. The next visit on 7th Sept. will be to GYVA Studio at 22 Bendigo St. Richmond. The time at the studio is 8.45 p.m., or for those requiring transport meet at Victoria Parade at 8.15 p.m. Visits for October and November will be announced when finalised.

In a note from Ian L3008, he requests information for the compiling of a list of frequencies such as services as the following: Bush Fire Networks, School Broadcasts, Forest Commission, Ship-to-Shore, Fishing Boats, Lighthouses, Citizen Frequencies, Model Aircraft, Firearms, Boats, Aircraft, Aircraft-to-Ground, and other frequency users operating in the range from 1.8 Mc. to 30 Mc. Details required are the exact frequency, time of operation, location, call signs, type of service, and other details which would assist in reception of the signal. This information can be forwarded to him direct, the address is good in any Call Book, or to me.

Those who assist will be forwarded a free copy when it is completed. We do not want broadcasting stations as there is enough information on these signals.

You're truly has not been listening very much on the DX bands due to being bitten by the v.h.f. bug, and has been listening on 2 mcs. To date have only received DX stations at Ballarat, being VK3ZER/M at Mt. Buninyong, received here with a 5 by 5 signal. He was using a four element beam three feet above the car and was running 8 watts to a 312. He worked about a dozen Melbourne stations without any trouble.

SOUTH AUSTRALIA

It seems that the S.W.L. Group in Mount Gambier is fast turning into a V.H.F. Group. It is hoped by the end of the year that there will be three more Limited Licences in Mount Gambier, due to three members sitting for a 2 call licence at the recent exam. Those who were John Lettman, Trevor and Colin. All that is to be done now is to wait for the results.

Listening at Colin's QTH has been mainly on 6 mcs and a little on 2 mcs. On Sunday, 15th July, there was an extremely good opening on 6 mcs to VK4, VK3 and VK7—a total of 25 distant stations were logged during the opening. The converter used was a r.f. unit type 26 which is on loan with a xtal locked converter is completed. The antenna was a 6 mcs is only a temporary three element yagi about 15 to 20 feet high. All stations heard during the opening were all running 5 + 4.

Gary VK3ZGR spent his first day 8 mcs on 15th July and worked seven VKs and two VK3s and Dale VK3ZER, ZL2GG was heard but not contacted. Gary was then running 6w and later on the power was increased to 15w. Input to a pair of p.p. 807s. The antenna used is a four element yagi about

40 ft. high. Gary's operating frequency is approx. 55.25 Mc.

Dale VK3ZER is running roughly 15w. input to a 832A, but at the moment is having trouble with his converter, but did manage to hear a few stations during the opening. The 6 mcs band came good from 1000 hours till 1800 hours and there were still stations audible when it came time to pull the big switch at 1800 hours.

Colin's three tube converter for 6 mcs is progressing very well and should be in operation very soon. The converter consists of a 12AT7 osc., 6X5 mixer, and a 8258 1.f. amp, which will feed into the Edystone 640 at 7 Mc.

SAVING MAIL

I wish to thank the following for their letters: Eric Treblecock, Chas. Abernethy, Peter Drew and Ian Thomas.

QSLs received by Eric L3043 so far include HC41E, OK3UD, 730AL, UH3ES, UDKAB, UHKKAA, VE3KE (3.5 Mc.), VK3ER, W9WIV (3.5 Mc.), ZC4PB and ZL3BAH. It may interest you to know chaps that Eric has mailed out 800 reports this year which is not bad going.

Chas. L3211 reports that s.w.f.ing has been out for a while, although he did log Oscar 2 on 148 Mc. on six occasions, and has sent logs away to California and hopes to receive confirmation in due course. Chas. has had his son home from VK3 so the Ham station has been working hence no s.w.f.ing.

Peter L3021 has recently acquired a new rx, which is mainly being used for overseas broadcasting stations. It covers 350 kc. to 8.5 Mc. in four bands and then has another six hand-picked coverage on the 21, 24, 28, 35, 48, and 11 mcs broadcast bands. This of course is very good for the use stated above with good results, however it also covers 160, 80, 40 and 15 mcs Amateur bands which is a great advantage, especially 15 mcs which Peter has not been able to receive before. This band comes

in on the 13 mcs band coverage. The rx is a nine-tube superbet, put out by Pye.

Band conditions in VK3 have been poor but 15 mcs has been fairly good for W, JA, VS, ZS, ZE and CHT in the afternoons, 20 mcs has been fair for VE and W in the afternoon, while 40 mcs is good for Ws on c.w. in the morning and good in the late afternoon and early evening for Ws on a.n.b., also JA and even DU, KXs, KXs, VRIG and one rare one —KXICV (7 Mc. a.n.b.). On 80 mcs, ZLs have been fading in and out on 40 and 80 mcs.

Ian L3055 is still finding time to listen in and has sent out 123 QSLs since March and has received so far 14 in return. The latest were VK3UD/LH, CNIRK, KLTN and ZL3OX for 109 mcs c.w. report. Ian has not logged too many countries or DX stations in the past month due to being busy at his studies, however he has managed to manage the 5 mcs converter in action again after blowing all the dust out of it and logged a few weak locals on the band. It seems a 6 mcs quad will have to be erected and also may get to work on the 6 mcs tx again, during the meantime it is hoped to see a rise in the DX total during the next few months.

So 13, and best of DX, Robert L3076.

DX LADDER FOR SEPTEMBER

	Countries	Zns.	S&B	W
Conf.	Hrd.	Conf.	Hrd.	St.
E. Treblecock	877	228	40	—
P. Drew	361	168	30	—
A. Wescott	34	208	31	89
M. Hillard	40	310	33	105
M. Cox	40	315	35	128
C. Abernethy	41	320	35	—
N. Harrison	36	314	34	—
P. Drew	33	310	34	—
P. Field	33	310	34	—
I. Thomas	33	314	34	—
D. Jenkins	10	141	7	—
H. Burger	8	185	3	19

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Sub Editor: **BUD POUNSETT, VK2AQJ,**

6 Alice Street, Queanbeyan, N.S.W.

ADDRESS CORRESPONDENCE FOR THIS PAGE DIRECT TO THE SUB EDITOR

A NEW BALANCED MODULATOR

Arrie Bles, ex-PA8FM, supplied the circuit and information on this balanced modulator. Arrie now lives at Springwood and hopes very soon to be back on the Amateur bands with a VK2 call sign. A friend of Arrie's, Mac van Schagen, PA2LZ, developed this circuit to overcome the difficulties in obtaining and maintaining balanced circuits associated with most balanced modulators. It was published in CGPA magazine and is used extensively in Holland. Fig. 1 shows the circuit of this unique balanced modulator having unbalanced input and output circuits. Impossible? This is how it works.

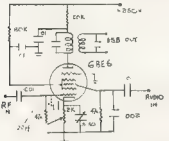


Fig. 1.—A New Balanced Modulator.

Any tube with three grids will work, but a type 6SA7 or 6BE6 pentagrid converter will perform best. A carrier signal of one volt maximum is applied to grid No. 1. As the cathode resistor is not bypassed, a large portion of the signal will appear across this resistor, approximately 85 volt. This produces a plate current of $85 \mu \times (1.0 - 0.8) \text{ mA}$. 85μ being the mutual conductance of grid No. 1 and $1.0 - 0.8$ or 0.2 mA , being the signal voltage between grid No. 1 and cathode.

Grids 2 and 3 are grounded for r.f. With 8.9 volt of r.f. on the cathode, the effect of grids 2 and 3 on the plate current would be as though this voltage was applied to these grids. In other words, in relation to grid 2 and 3, the tube is operating in grounded grid. The result is that another r.f. plate current will flow amounting to $-(85 \mu \text{ plus } 85 \mu) \times 0.9 \text{ mA}$. 85μ and 85μ are the mutual conductances of grids 2 and 3.

If these two r.f. plate currents can be balanced, they will cancel and no r.f. plate current will flow, resulting in no r.f. plate voltage. The carrier will be suppressed in

the plate circuit. The carrier suppression can be adjusted with the cathode potentiometer. This adjustment has greater effect on the grid No. 1 to ground voltage than the grids 2 and 3 to ground voltage, making the balancing control easy to use. To make the balance perfect, phase-correction is required. A small trimmer capacitor across the cathode resistor is used to accomplish this. If, however, complete carrier suppression cannot be attained with the trimmer capacitor and less capacitance than the minimum is required, a small capacitor will need to be connected between grid No. 1 and cathode. Audio modulation is applied to grid No. 3, unbalancing the circuit at audio frequencies, so producing two sidebands in the output.

Using a 6BE6 tube and applying 0.5 volt of r.f. and audio, a peak d.s.b. voltage of 8 volts can easily be obtained in the plate circuit. Some manipulation of screen and plate voltage may be necessary. Keep the screen voltage fairly low. With the large cathode resistor and large grid No. 1 bias voltage, d.c. plate current can be expected to be less than 0.5 mA. Typical circuit values are given in Fig. 1. Many thanks go to Arrie for this very interesting circuit which will probably become known as the FA0 balanced modulator and should prove to be very popular.

R.S.G.B. AMATEUR RADIO HANDBOOK

Chapter 10 of the current R.S.G.B. Handbook is entitled Single Sideband and in forty-one pages a very well illustrated volume provides the reader with an excellent short course on s.s.b. transmitting and receiving techniques. The text is easily read and understood so that those Amateurs with a sketchy knowledge of sideband will find this a good place to begin their search for knowledge of this subject. The reader is taken through by step by step discussion on the fundamentals from how to suppress the carrier and produce a sideband to linear amplifiers and how to test them. At all times the emphasis is on the practical application of these principles and no great knowledge of mathematics is required.

Examples are given of actual designs of both filter and phasing excitors, while the "Third Method" is described in theory only. Linear amplifiers are adequately treated both in theory and practice, there being several circuits to suit the Australian Amateur, from the man who wants a modest final to those who want the limit.

If you are a keen sidebander, new or old, here is a worthwhile manual to add to your library.

S.S.B. NOISE LIMITER

Effective noise limiters for single sideband reception are few and far between. The one marketed by Collins Radio while doing a good job, has a high price tag hanging from it.

Ron Harrison, VK4AHJ, has come up with the noise limiter shown in Fig. 2. Ron uses this limiter in his 20 mc mobile s.s.b. receiver and finds it very effective. It works best at low levels so should follow immediately after the detector, and before the volume control. The threshold clipping level is adjusted by the 10K potentiometer.

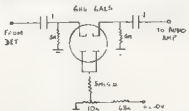


Fig. 2.—Noise Limiter.

SOME DEFINITIONS

The last two issues of the "Mullard Outlook," Australian Edition, Vol. 3, Nos. 1 and 2, have contained an interesting discussion on the fundamentals of s.s.b. Those of you who have not yet become familiar with some of the terms used frequently by sideband opera-

tors will find the list of definitions of assistance. Here, for those more seasoned s.s.b. operators, some of the commonly used terms are defined. Give these a little thought, it could lead to better operating practices.

Automatic Load Control: A means of maintaining a signal level adjusted so that the power amplifier works near its maximum power capability without being overloaded on signal peaks.

Break-In: The ability to break-in on a transmission during pauses in the sending station's transmission.

Linear Amplifier: An amplifier whose output is always proportional to its input.

Load Comparison: A circuit technique used to indicate correct loading.

Modulation Envelope: Envelope of modulated signal. When recovered by rectification, it is the modulation of an a.m. signal. In s.s.b. the rectified envelope does not represent the modulating signal—the carrier must first be re-inserted. Envelope of s.s.b. signal is of prime importance in determining the limits of linearity and power of an amplifier.

Product Detector: A type of demodulator, in operation somewhat analogous to the mixer in superheterodyne receiver. Usually preferred for single sideband reception detection since it minimises intermodulation distortion products in the audio output signal and usually requires a low amplitude local oscillator signal.

Shape Factor: The ratio of the bandwidth of a filter at 40 db. to its bandwidth at 3 db.

The definitions in this item were taken from the March-April "Mullard Outlook," Australian Edition, and our thanks go to the Editor of that publication.

W.I.A. N.S.W. DIVISION

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U200/12	1-24	4-20	13.75	10.4	15 or 20	30*	6.5	2.75
U200/12	1-24	14-20	13.75	10.4	15 or 20	40*	6.5	1.00
U200/8	1.1-206	20-206	17	15	8	20†	8.78	1.49
U200/10	1.1-206	20-206	17	15	10 or 15	40†	9.06	1.50
U240/12	10-240	25-240	14	11	15	30*	8.0	6.00
U300/8	10-400†	14-400	22	20	8 or 10	40†	9.188	1.50

* up to 30 Mc/s

† up to 20 Mc/s

‡ Slight mechanical modification permits extension of range.

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